



# **HPC for the simulation of turbulent combustion in aeronautical engines**

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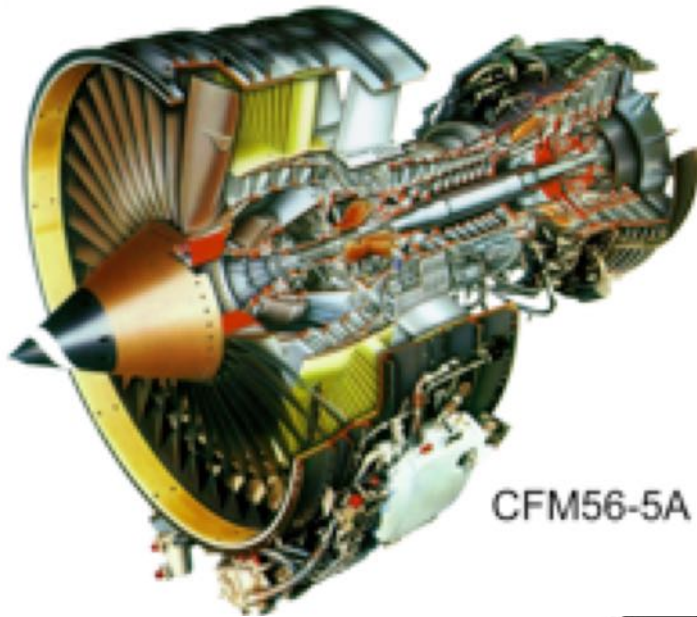
**Renaud Mercier – SAFRAN TECH, France**

**In memoriam C. Dobrzynski – LMB/INRIA Bordeaux**

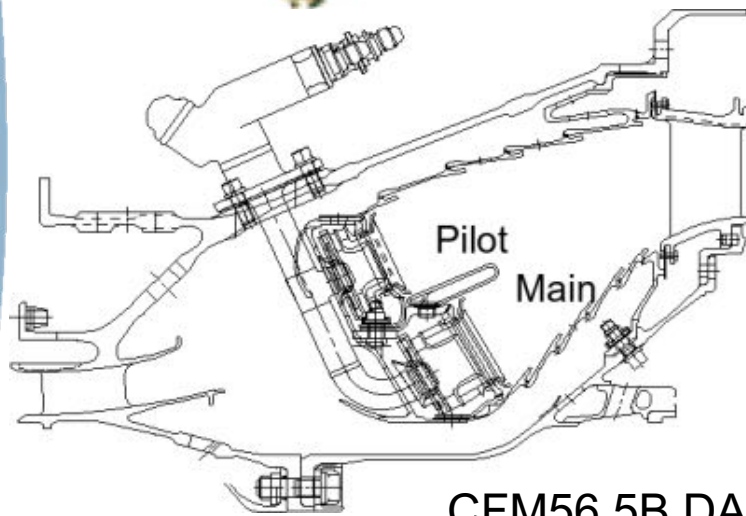
**PRACEdays18**

**29/05/2018 – University of Ljubljana - Slovenia**

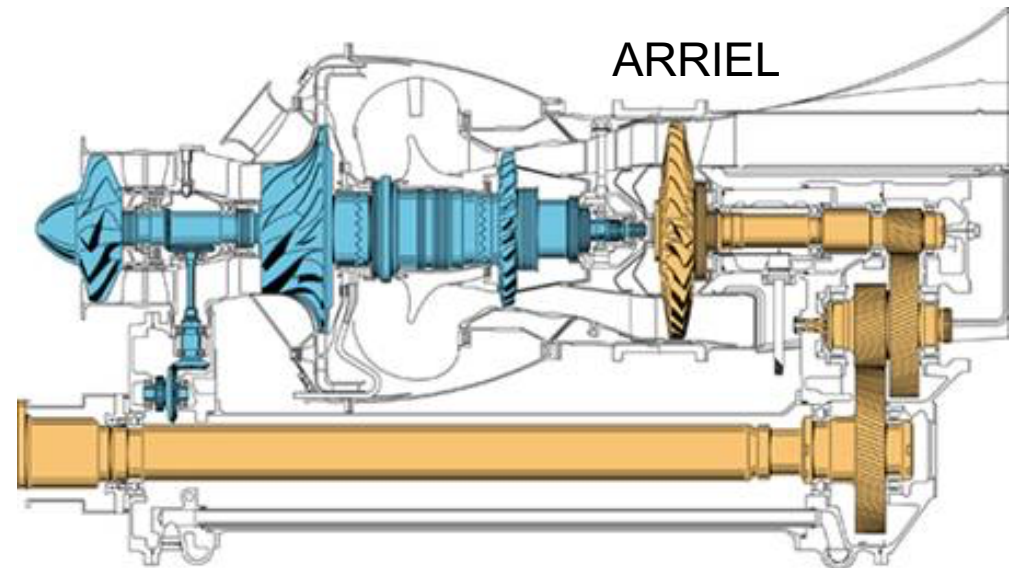
# ■ Aeronautical engines



CFM56-5A



CFM56 5B DAC



ARRIEL

# ■ Engine design is driven by two major constraints

## **Fuel efficiency**

- ▶ **Economic constraints**
  - reduced fuel consumption
  - reduced CO<sub>2</sub> emissions
- ▶ **Global efficiency of the engine**

$$\text{Turbofan} = \text{Ducted fan} + \text{Gas turbine (core engine)}$$

$$\eta_{glob} = \eta_{prop} \times \eta_{th}$$

**Propulsive efficiency**

**Thermal efficiency**

**High bypass ratio architecture**



**Ultra-high pressure ratio core engine**

$$\eta_{th} = 1 - \left( \frac{P_1}{P_2} \right)^{\frac{\gamma - 1}{\gamma}}$$

## **Pollutant emissions**

- ▶ **International regulations**
  - CAEP regulations
- ▶ **Main pollutants**
  - UHC
  - Smoke
  - Carbon Monoxide (CO)
  - Nitrogen Oxides (NO<sub>x</sub>)



**Smoke in the trail of a B-52**

**Ultra low-NO<sub>x</sub> combustion chamber**

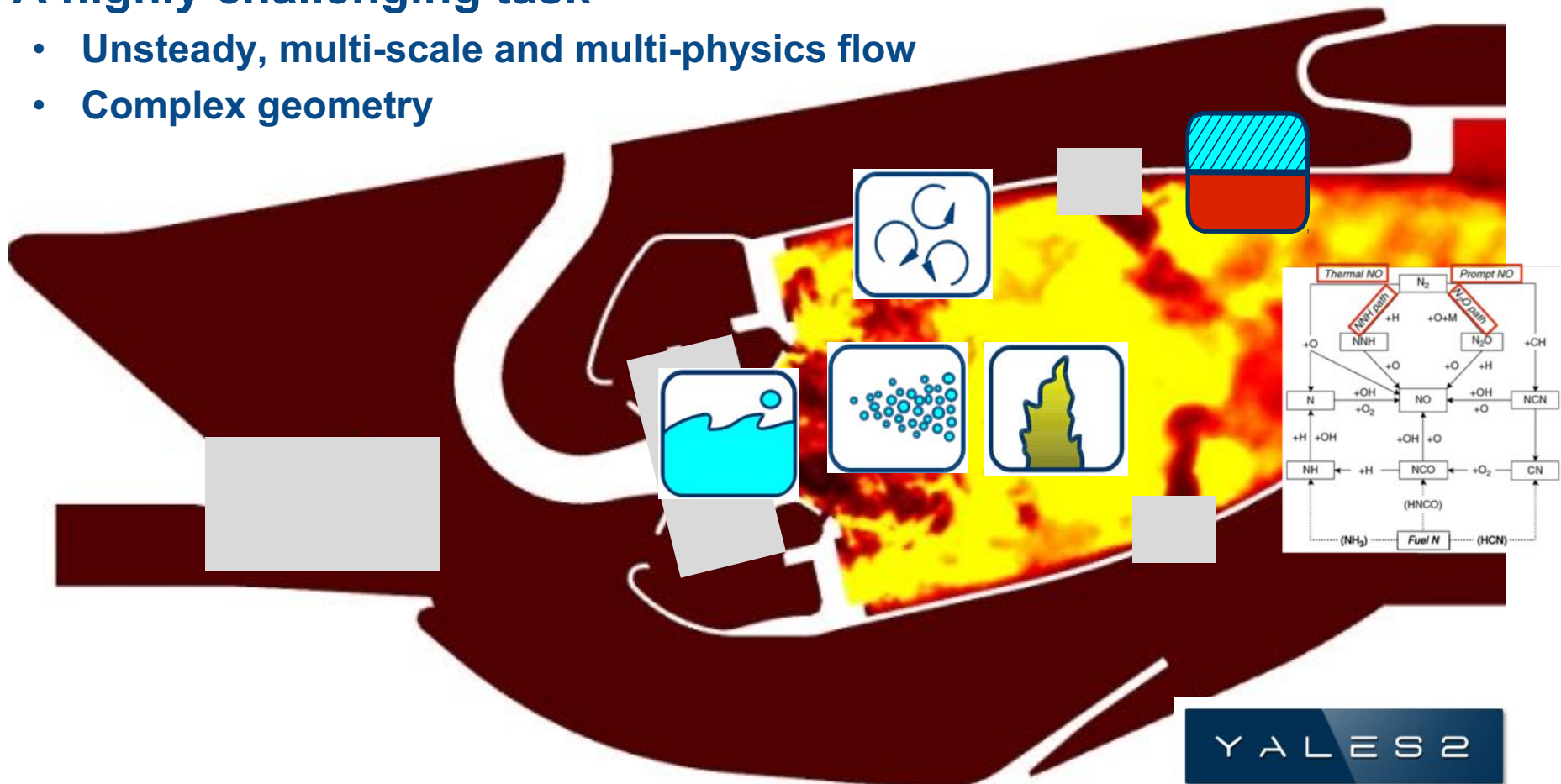




# Prediction of performances and pollutant emissions in aeronautical engines

## ► A highly challenging task

- Unsteady, multi-scale and multi-physics flow
- Complex geometry



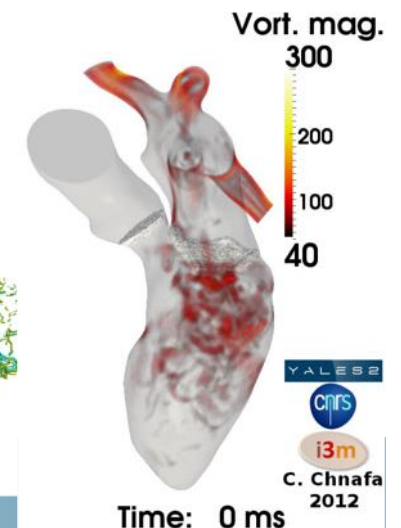
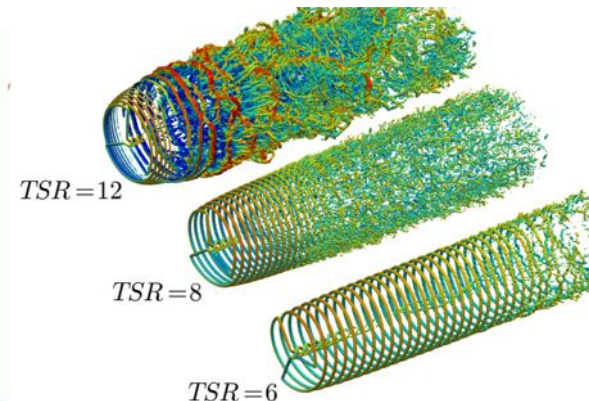
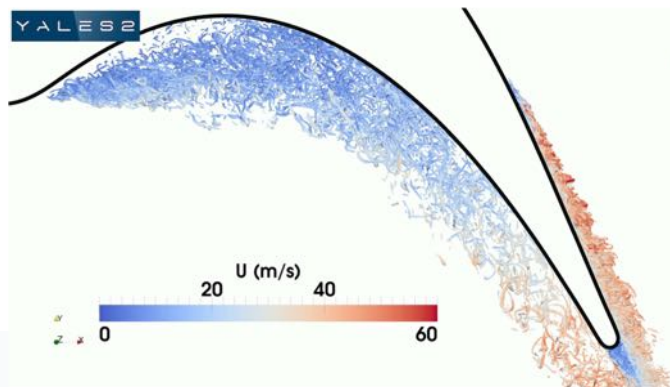
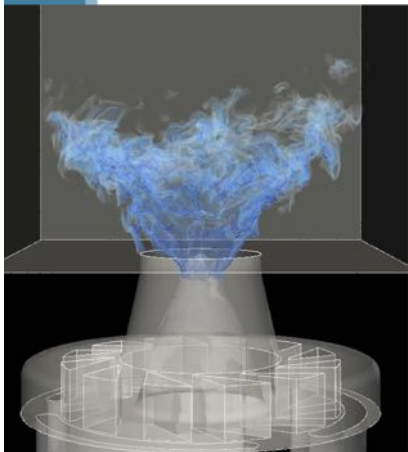
- Unsteady approaches are mandatory to predict these phenomena
- Objective: develop LES models for pollutant predictions

# Flow solver

Y A L E S 2

[1] YALES2 web site, <http://www.coria-cfd.fr>  
[2] SUCCESS web site, <http://success.coria-cfd.fr>

- ▶ Low-Mach number Navier-Stokes equations with projection method [1,2]
- ▶ Unstructured meshes with adaptive grid refinement
- ▶ 400k+ lines of object-oriented fortran2008
- ▶ MPI and hybrid OpenMP/MPI
- ▶ 4th-order central finite-volume method and 4th-order time integration
- ▶ Combustion modeling
  - Tabulated or complex chemistry, NOx prediction model...
- ▶ Two-phase flows
  - Spray modeling (Lagrangian particles)
  - Primary atomization (Accurate Conservative Levelset)
- ▶ Suited for massively parallel computing (>32 000 procs)

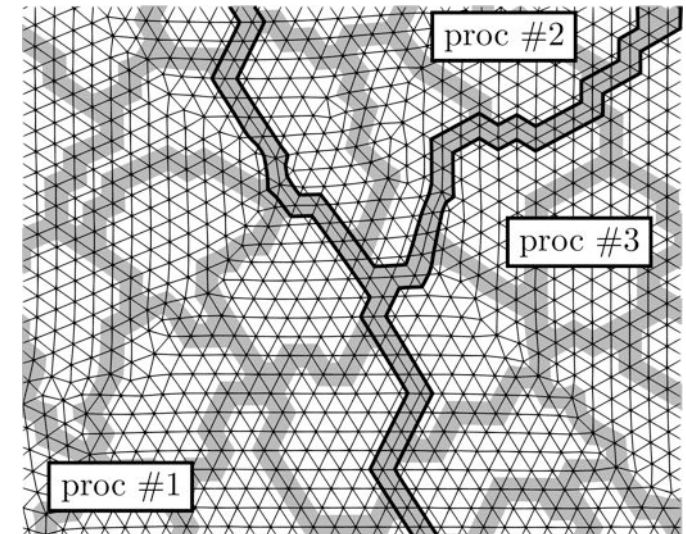
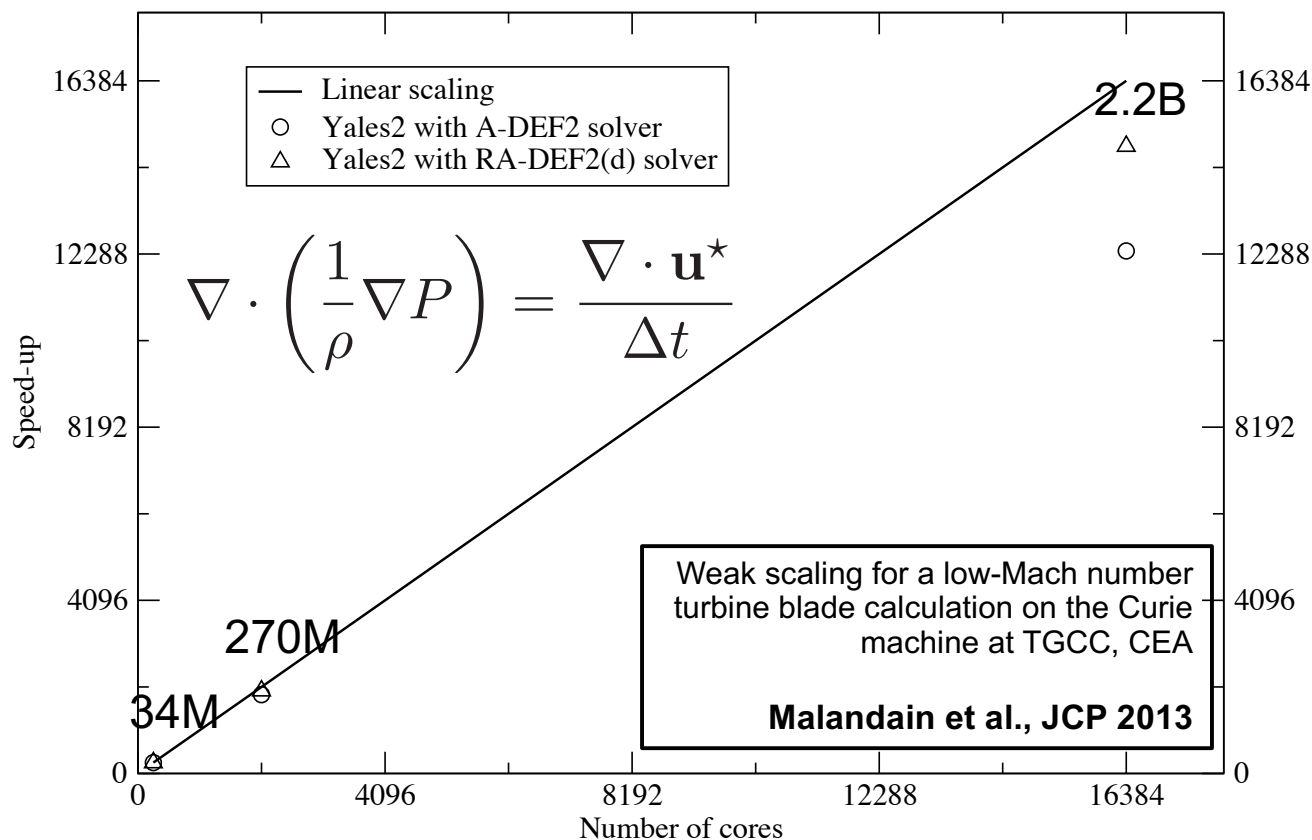


# ■ YALES2 in-core and parallel performances

## ► Two-level domain decomposition [1]

- Mesh is split into cell groups at the core level
- Enables to fit in L2 cache memory
- Used for the preconditioning of the linear solvers

## ► In-house linear solvers



# ■ The YALES2 network

- ▶ A collaborative network supported by the French combustion community
- ▶ More than 200 trained researchers and engineers

## **Academia**

**SUCCESS scientific group**  
(<http://success.coria-cfd.fr>):  
CORIA, CERFACS, IMAG, LEGI  
EM2C, IMFT, IFP-EN, LMA

ULB, MONS, UCL, LOMC,  
LMB/INRIA, Sherbrooke,  
PPRIME

## **HPC experts**

ECR lab  
INTEL/CEA/GENCI/UVSQ

## **Computing centers**

CRIANN, IDRIS, CINES, TGCC  
GENCI, PRACE

## **Industry**

SAFRAN  
(YALES2-AE)

ARIANE GROUP  
SOLVAY  
AIR LIQUIDE  
ADWEN

...

## **SMEs**

GDTech  
Paralgo  
Linterweb



# **Towards lean-premixed low-NOx burners**

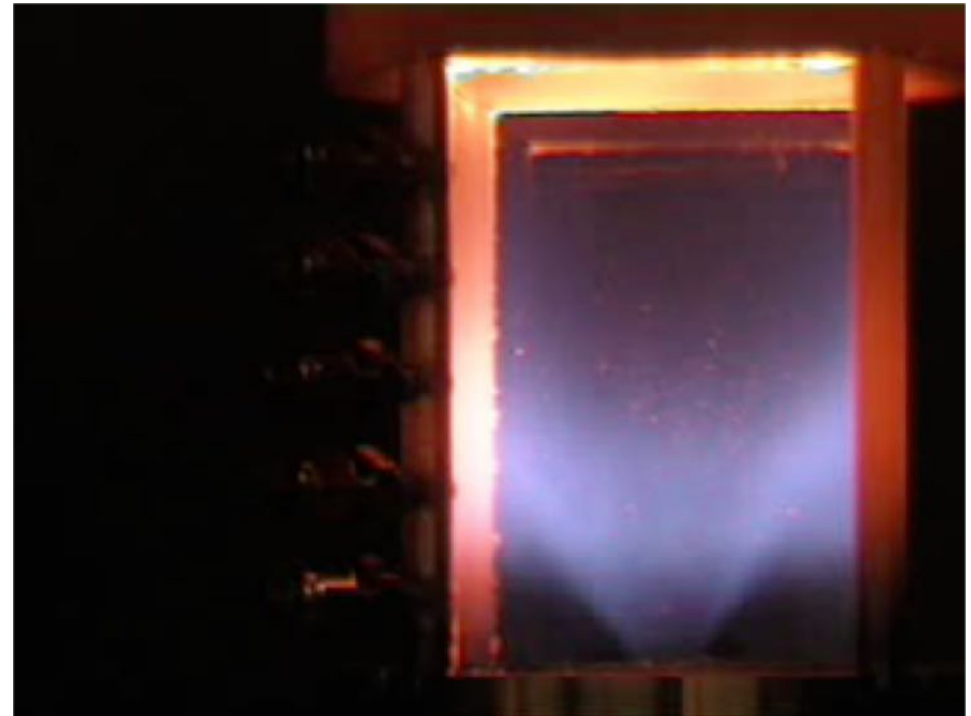
## **LES of the PRECCINSTA burner with finite-rate chemistry**



## ■ The PRECCINSTA burner (1/2)

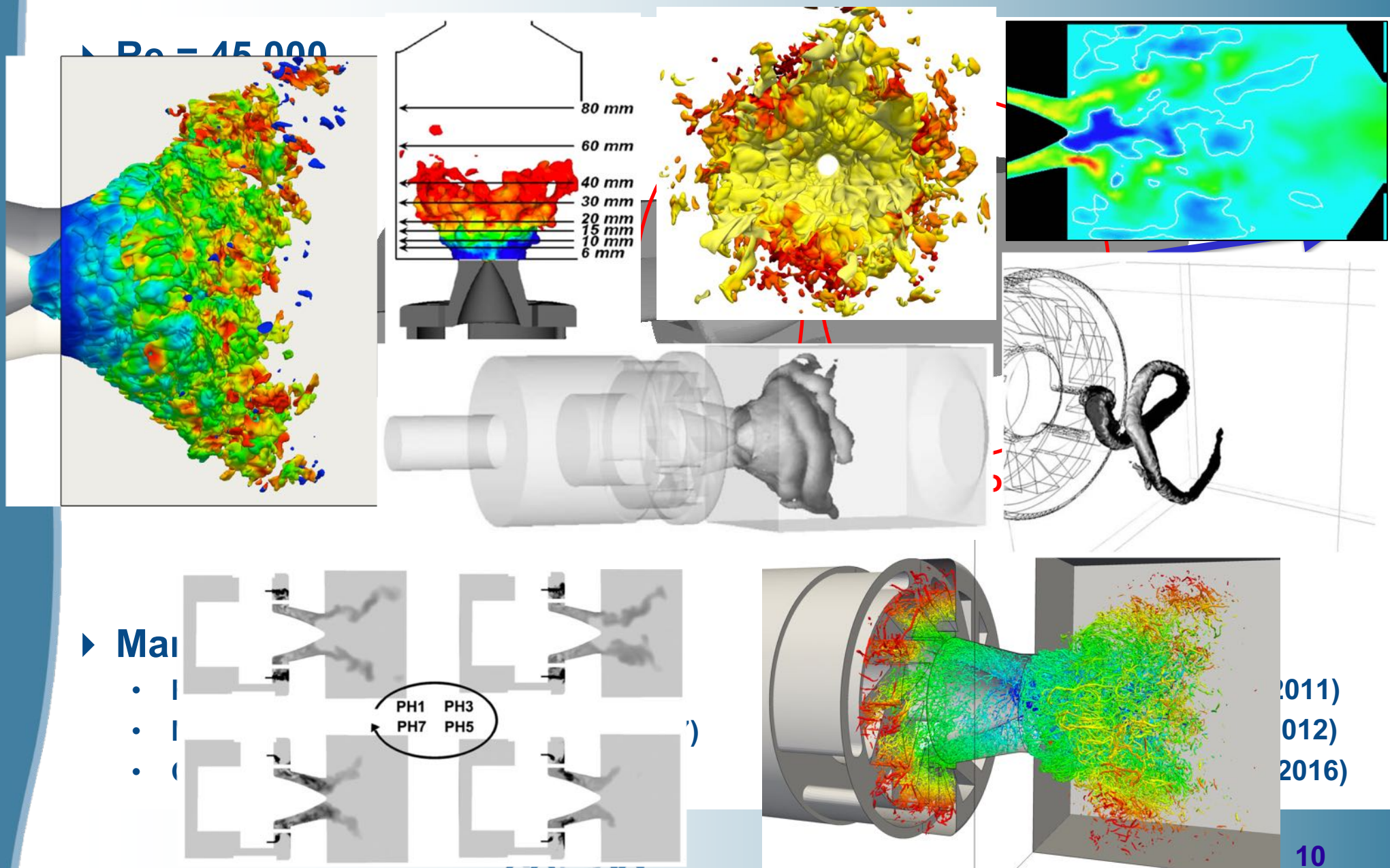
- ▶ Experimental lean-premixed CH<sub>4</sub>/air combustor with swirl
- ▶ Designed by SAFRAN Helicopter Engines (Turbomeca)
- ▶ Built to test LES capability for prediction of combustion instabilities
- ▶ Different equivalence ratios corresponding to stable or unstable regimes
- ▶ Non-intrusive measurements performed at DLR (Germany)

PRECCINSTA experimental burner



Equivalence ratio is decreasing slightly from 0.8 to 0.5

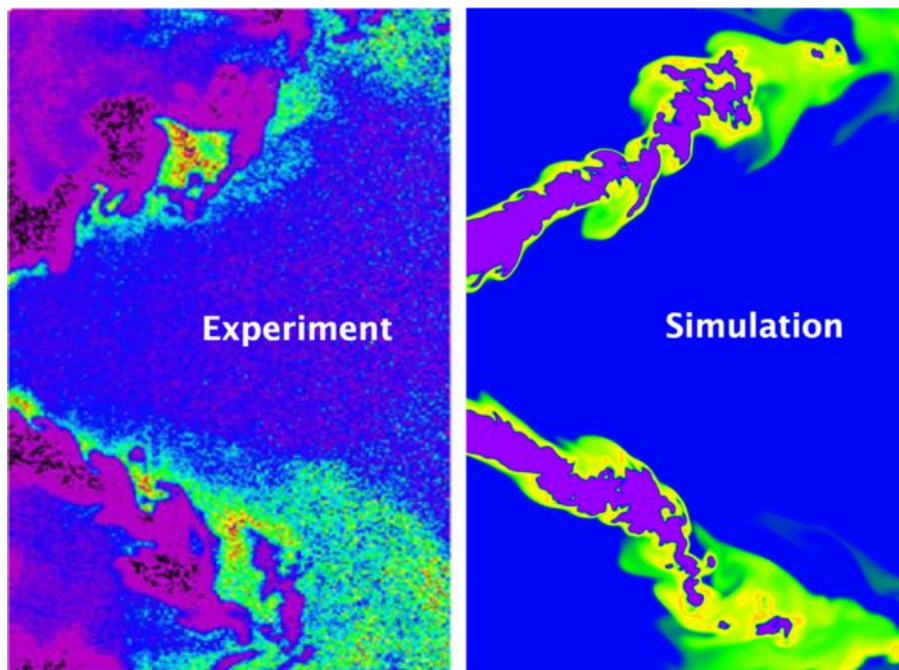
## ■ The PRECCINSTA burner (2/2)



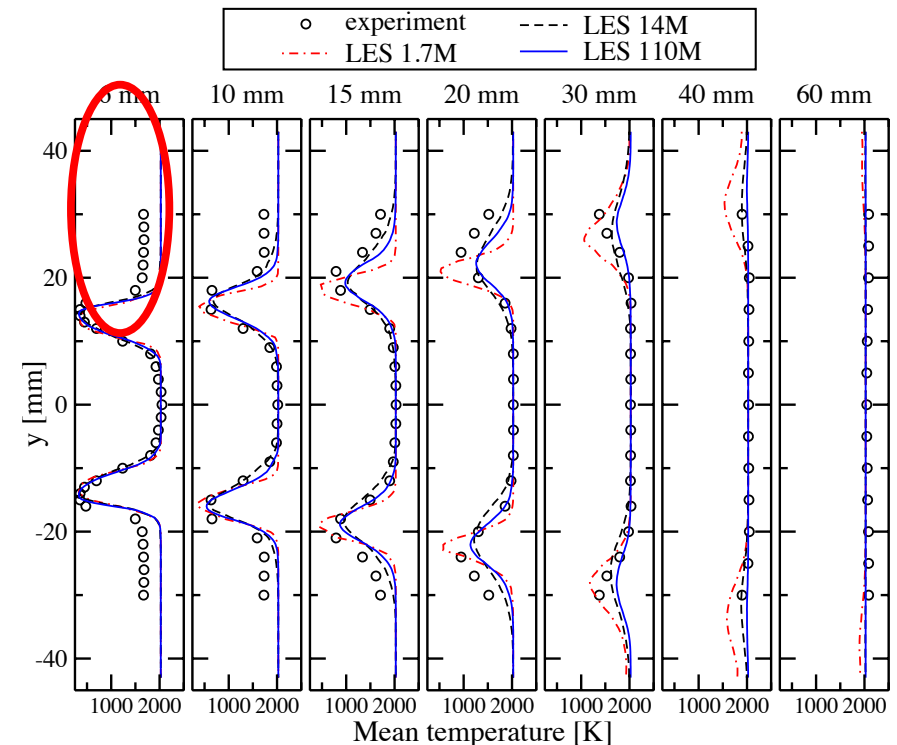
## ■ A remaining open question...

- ▶ No wall temperature/heat flux are available in the experiment
- ▶ Results from adiabatic simulations versus experiment

OH field



Moureau et al., C&F 2011



- ▶ V flame (heat loss) versus M flame (adiabatic) ?
- ▶ Difficult to model with tabulated chemistry => finite-rate chemistry



# ■ HPC for finite-rate chemistry

$$\underbrace{\frac{\partial \rho Y_k}{\partial t} + \nabla \cdot \rho Y_k \mathbf{u}}_{\substack{\text{transport} \\ 10^{-6} \text{ s}}} = \underbrace{\nabla \cdot (-\rho \mathbf{V}_k Y_k)}_{\substack{\text{diffusion} \\ 10^{-9} \text{ s}}} + \underbrace{\dot{\omega}_k}_{\substack{\text{reactions} \\ 10^{-12} \text{ s}}} \quad 10 \leq k \leq 100$$

## ► Key ingredients

### Dynamic TFLES model

- Allows to resolve the flame front on the LES grid (Colin et al. 2000)

### Operator splitting

- Each phenomenon is advanced at its own characteristic time

### CVODE stiff integrator

- Variable order and variable timestep integration with error control + analytical Jacobian + full vectorization of reaction rates and Jacobian

### Dynamic load balancing

- 2-level task sharing algorithm based on MPI (Fontenaille et al., submitted to EUROPAR 2018)

- ▼ Validated with up to 91 species and 700 reactions (kerosene/air combustion)
- ▼ Good performances up to 32'000 cores

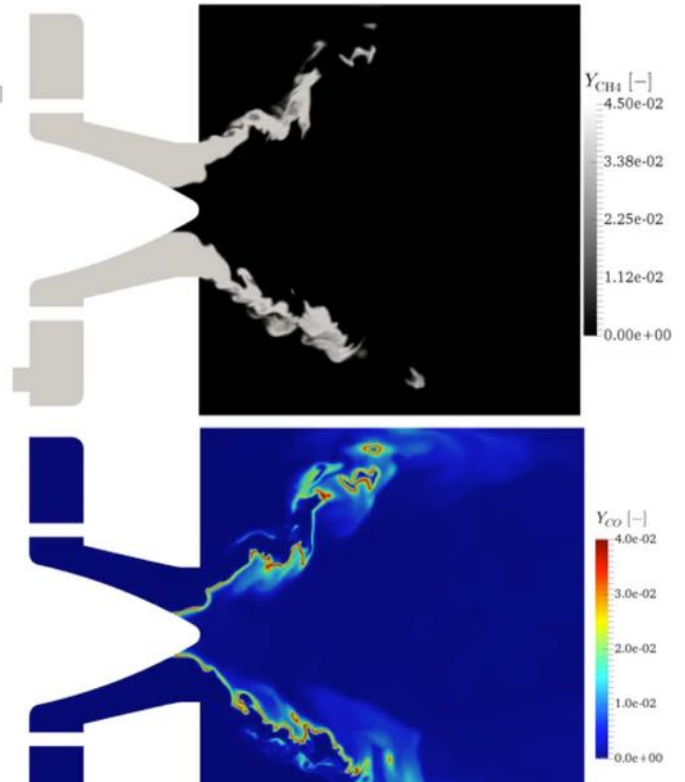
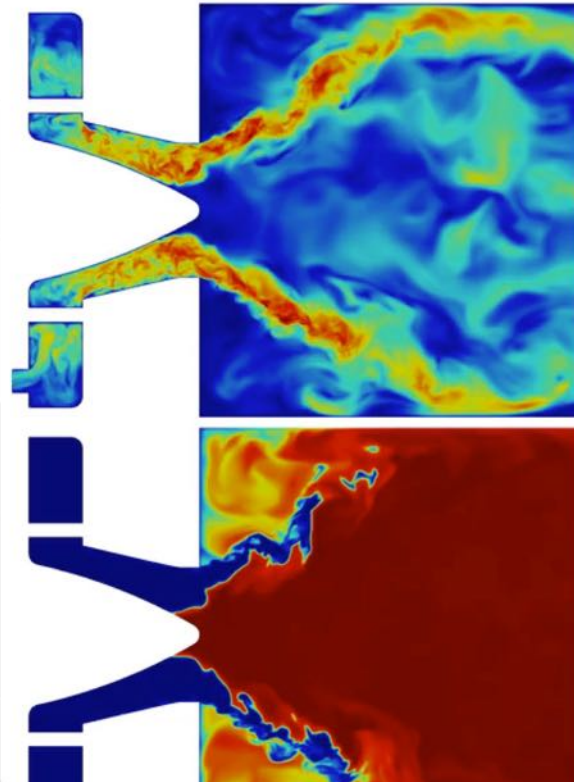
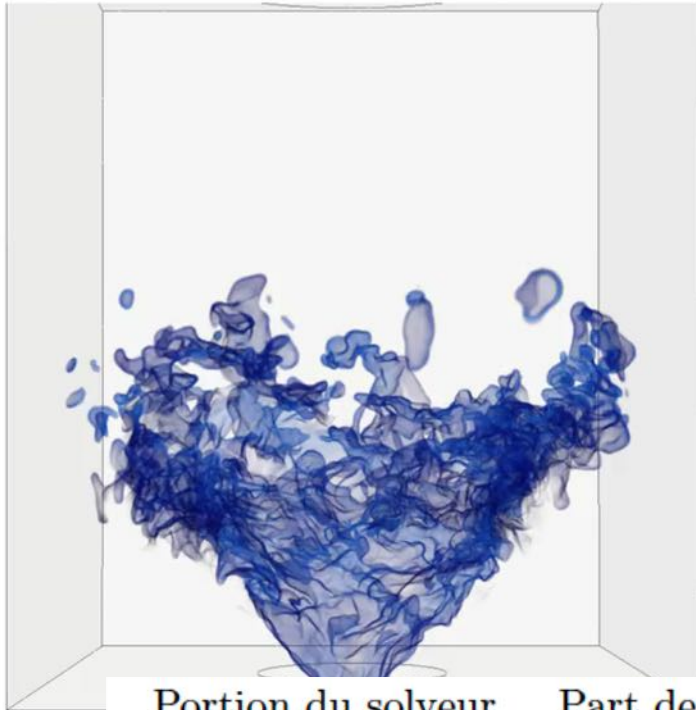


# Mesochallenge Myria 2017 @ CRIANN

## FIRELES PRACE project, 16384 cores on Curie

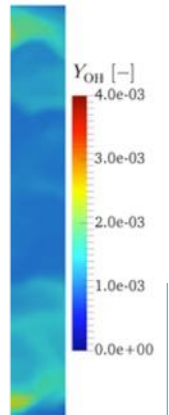
### PRECCINSTA burner

877M elements - Lu17 scheme - non-adiabatic walls



Portion du solveur	Part de la boucle temporelle [%]	RCT [ $\mu\text{s}/\text{noeud}/\text{iteration} * N_{\text{proc}}$ ]
Advection	0.78	6.5
Implicit diffusion	3.41	28.7
Pressure correction	8.48	71.2
Scalar advection	9.26	77.8
Scalar diffusivity	10.29	86.4
Scalar source term	16.62	139.6
Scalar diffusion	47.09	395.7
<b>GLOBAL</b>	<b>100.0</b>	<b>840.2</b>

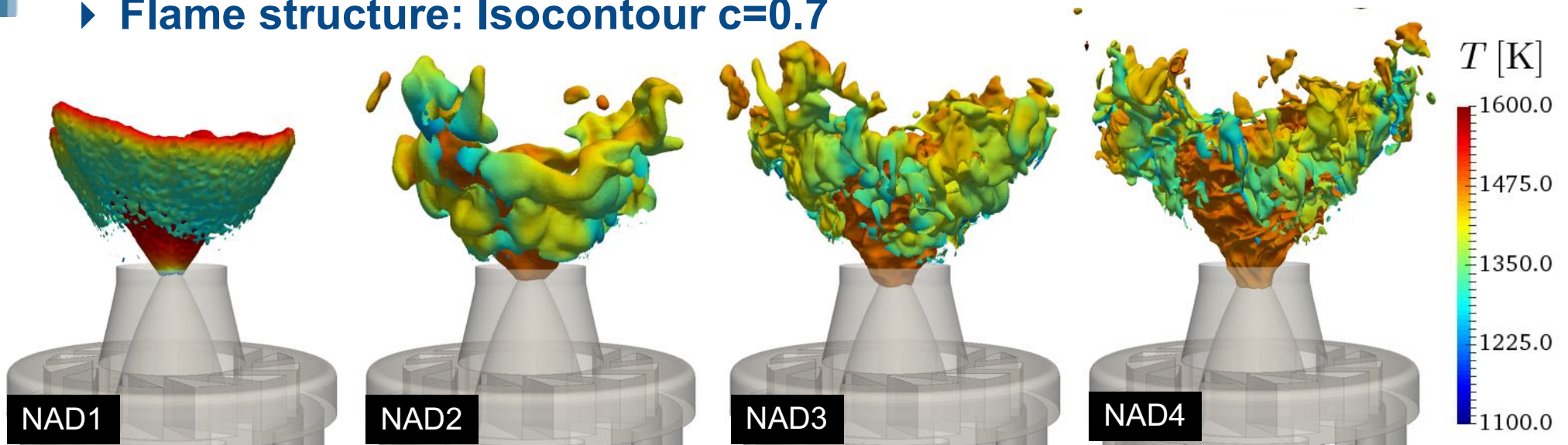
Only 17% of CPU  
time in species  
source term !



## ■ Non-adiabatic cases

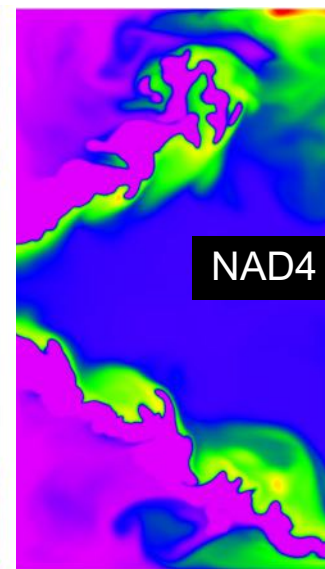
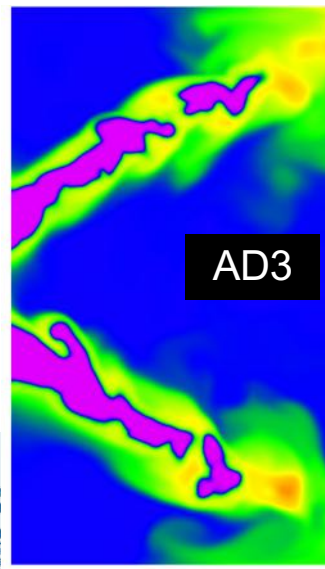
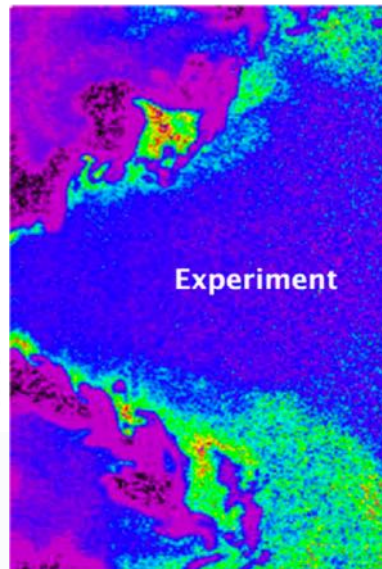
Mesh name	1	2	3	4
#cells [million]	1.7	14	110	877
Cell size [mm]	1.2	0.6	0.3	0.15
Heat loss/Total HR [%]	3.4	6.1	6.5	6.0

### ► Flame structure: Isocontour $c=0.7$



Complete extinction of external flame => V-shape flame

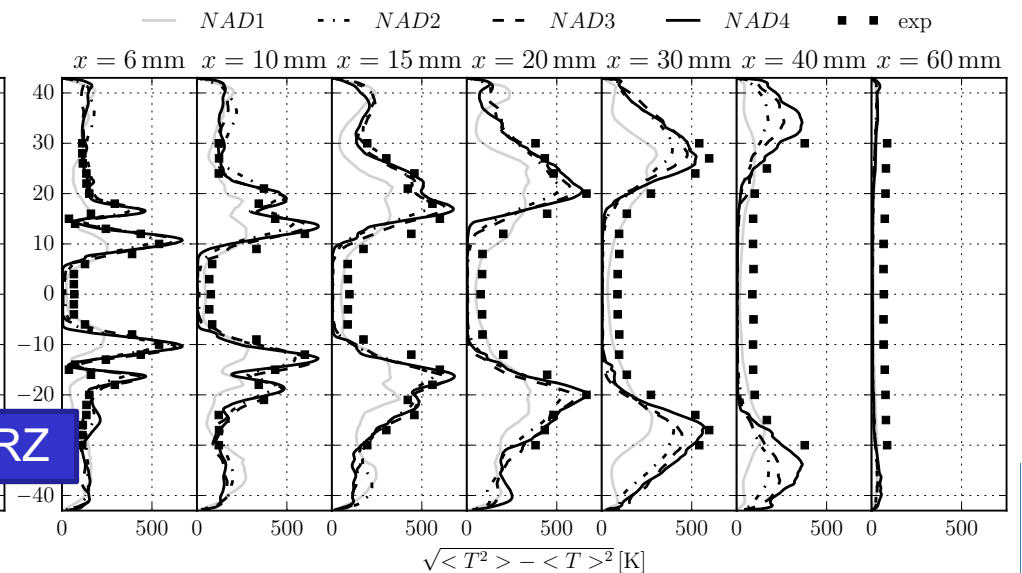
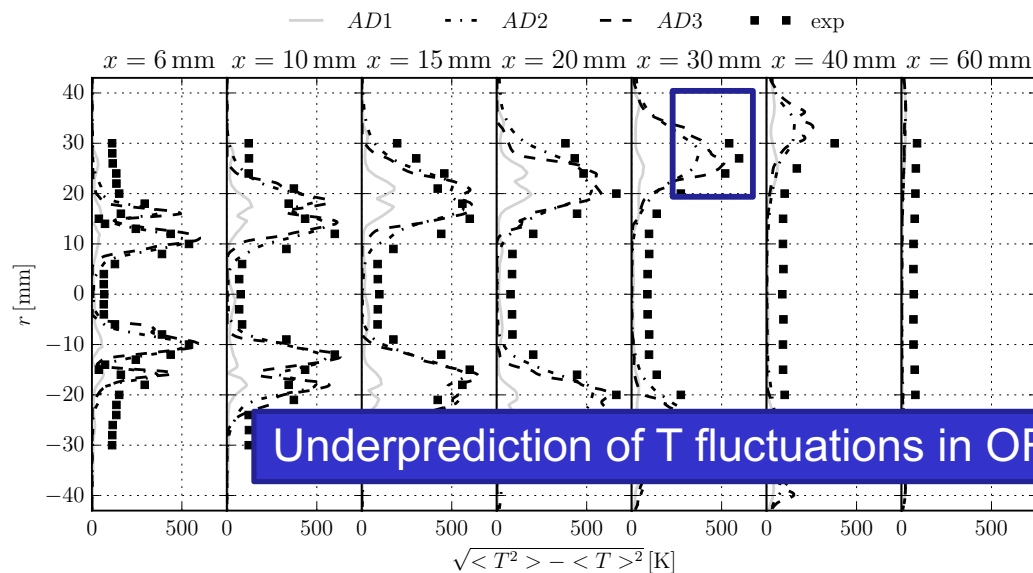
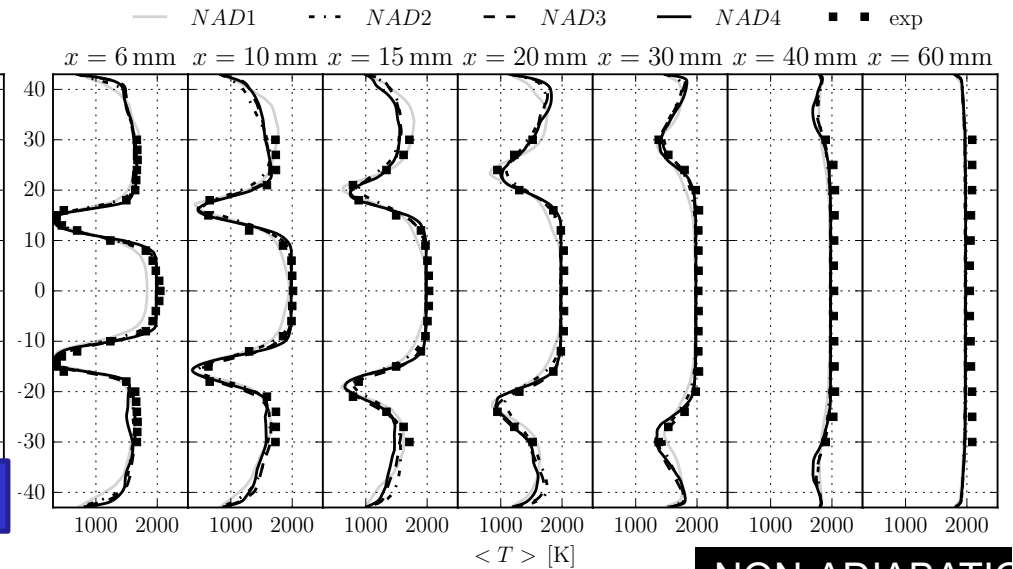
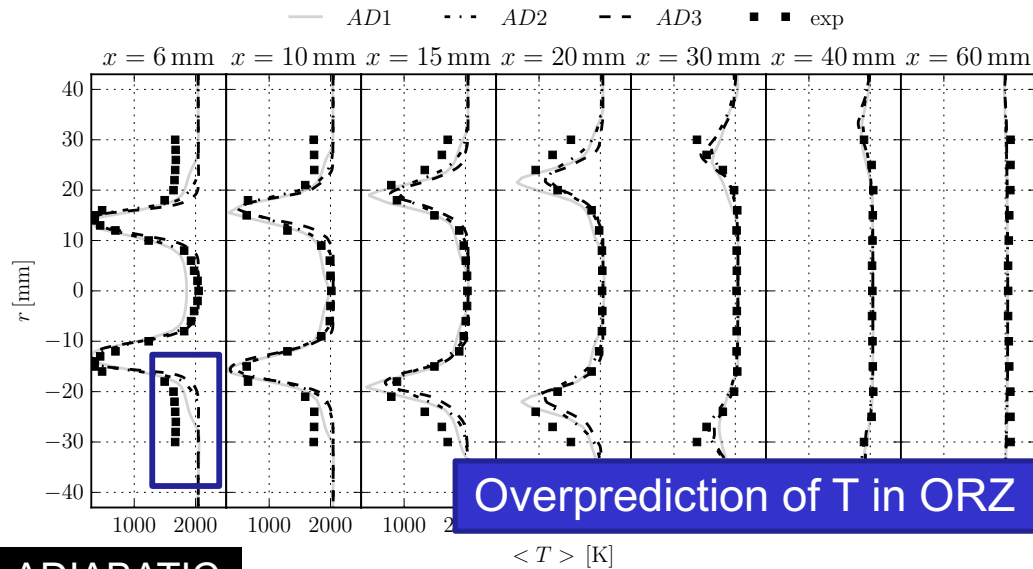
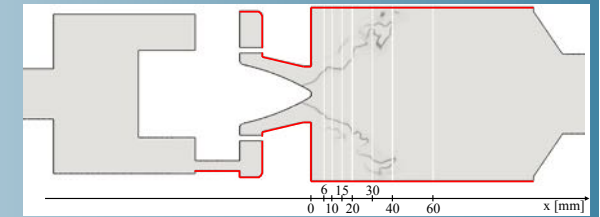
OH field



P. Bénard et al.,  
accepted to the 2018 Int.  
Comb. Symp., Dublin

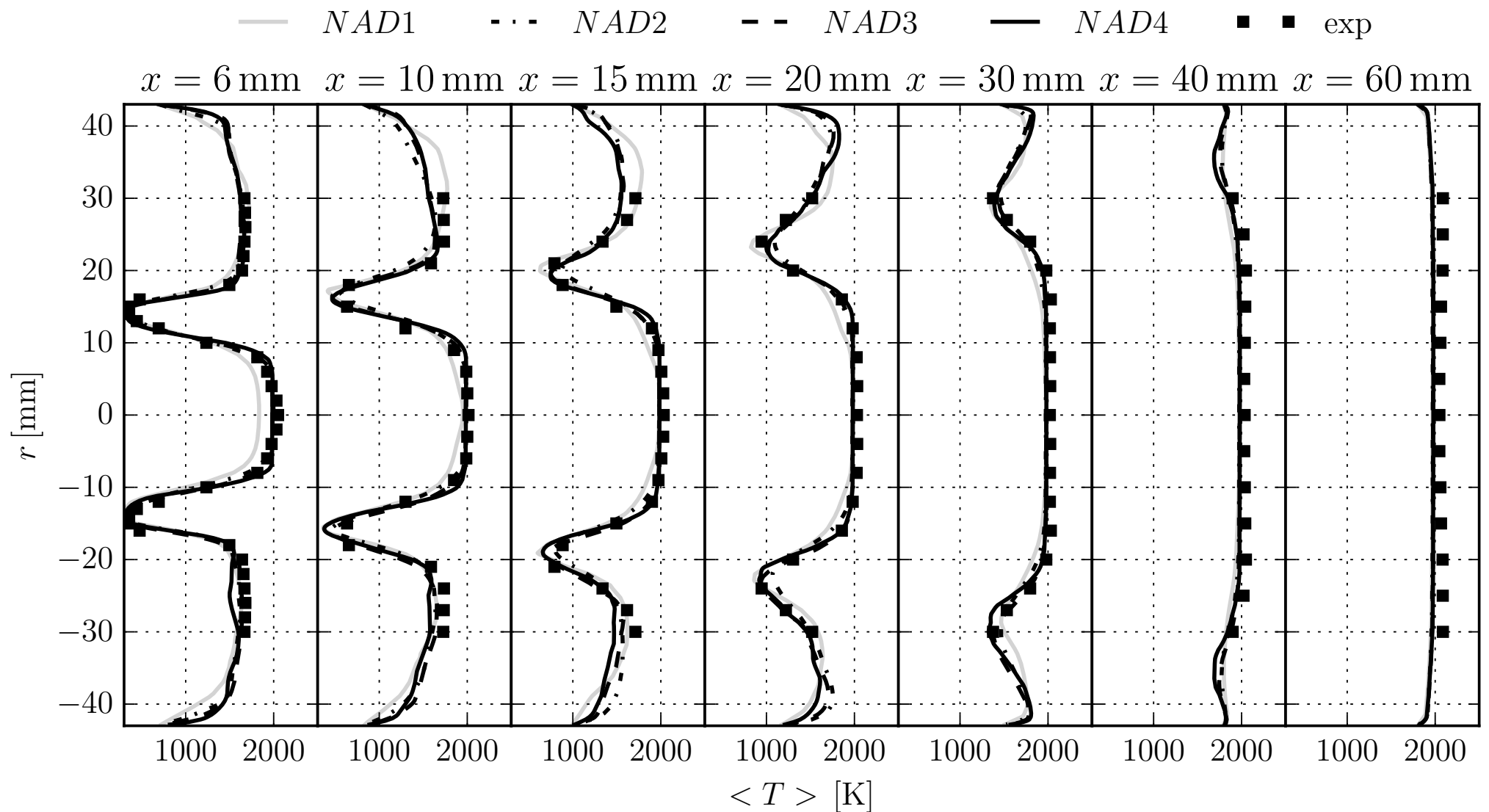
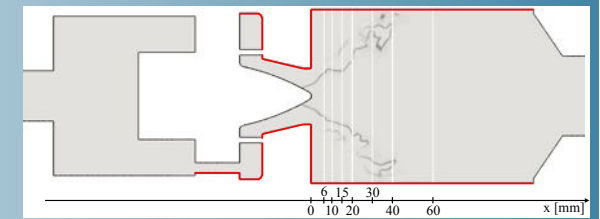


# Mean and RMS temperature



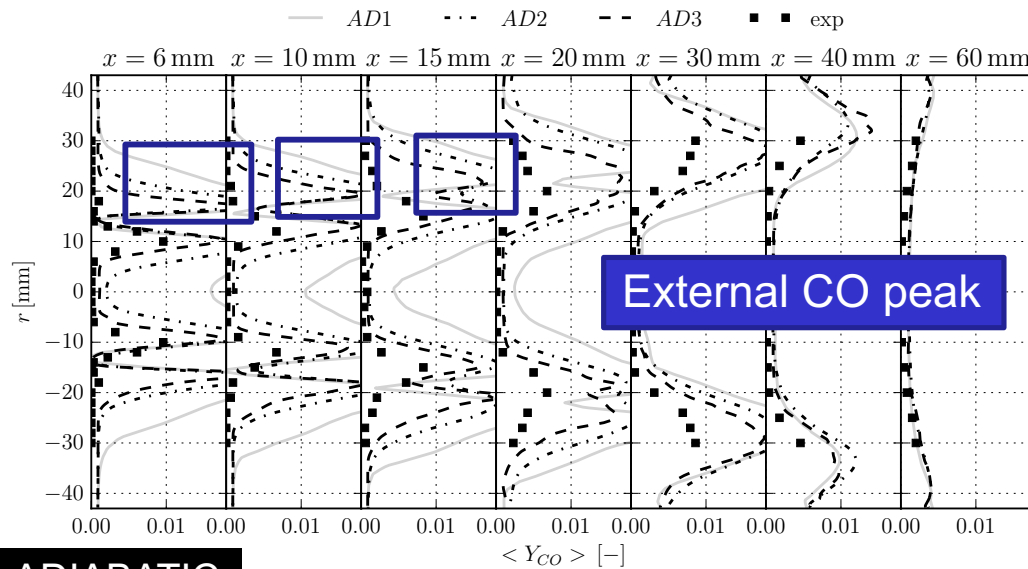
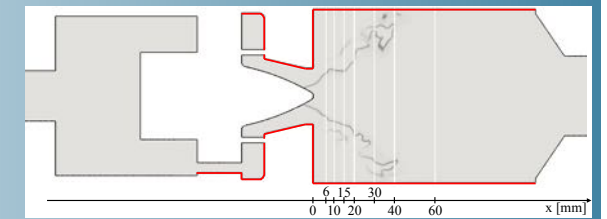


# Mean and RMS temperature

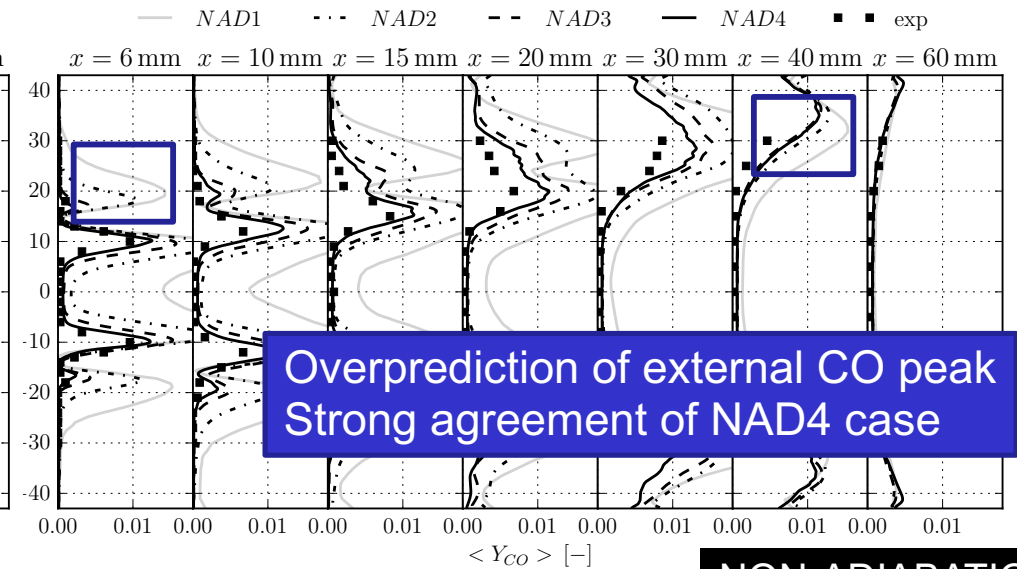




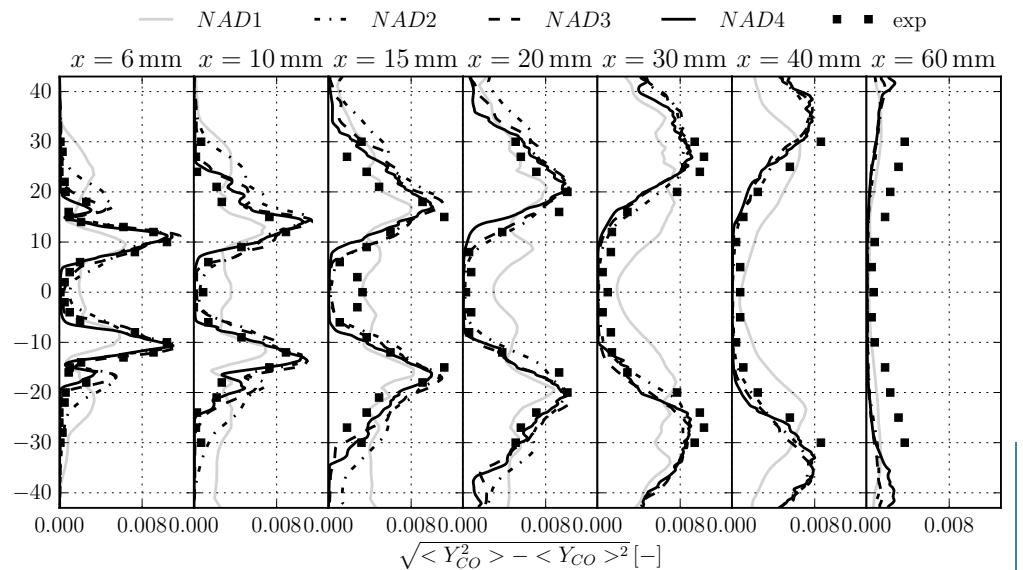
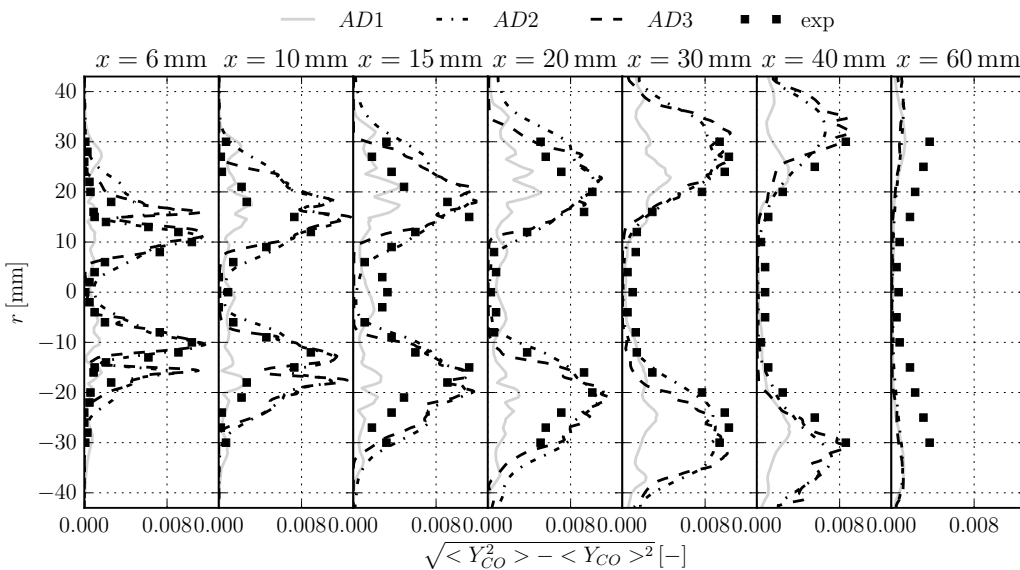
# Mean and RMS CO mass fraction



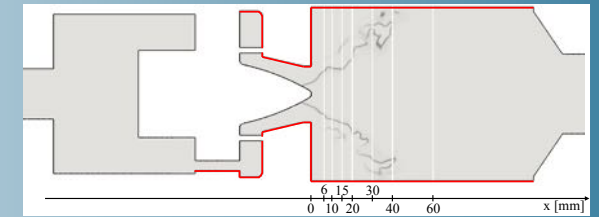
ADIABATIC



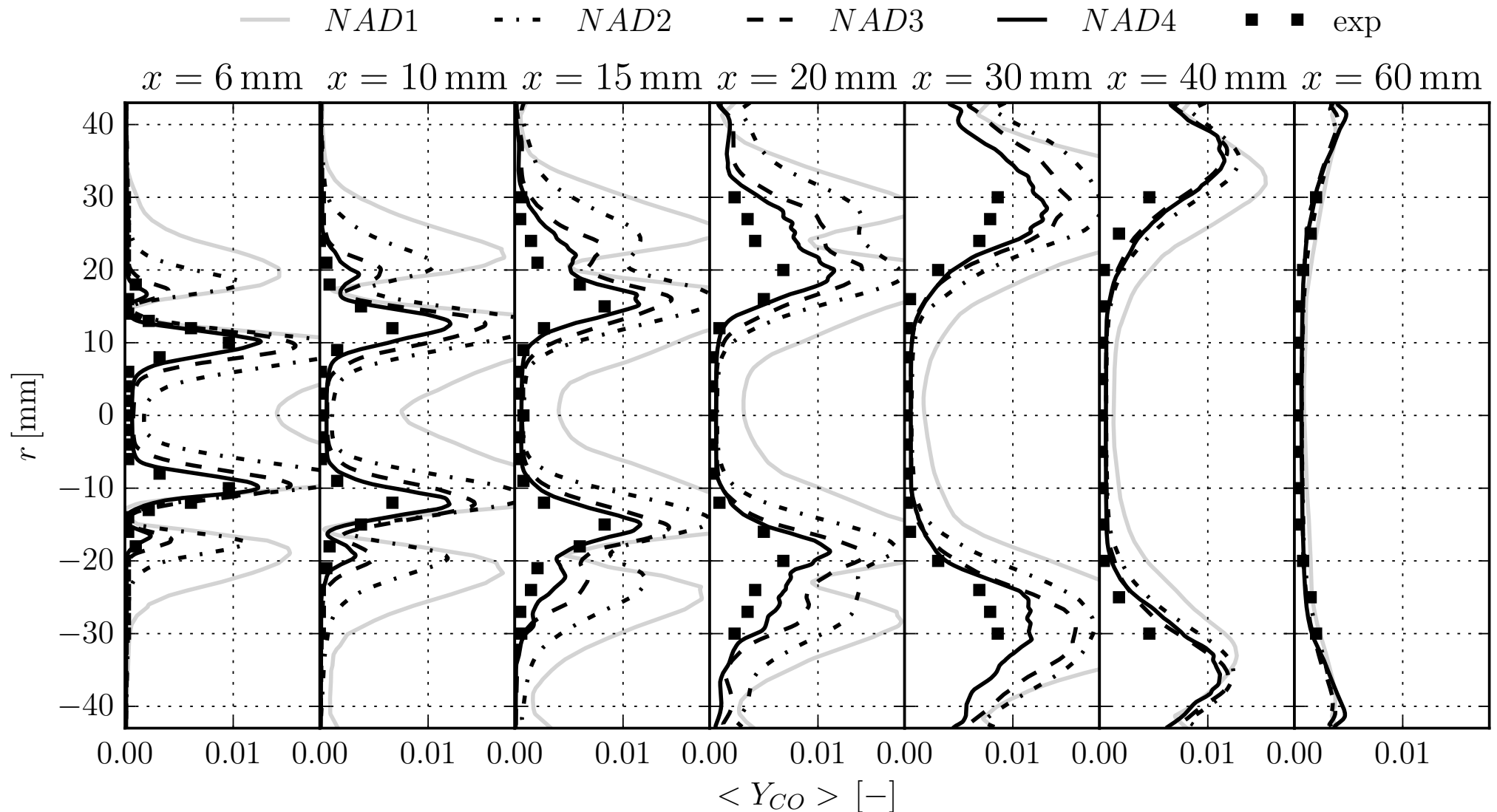
NON-ADIABATIC



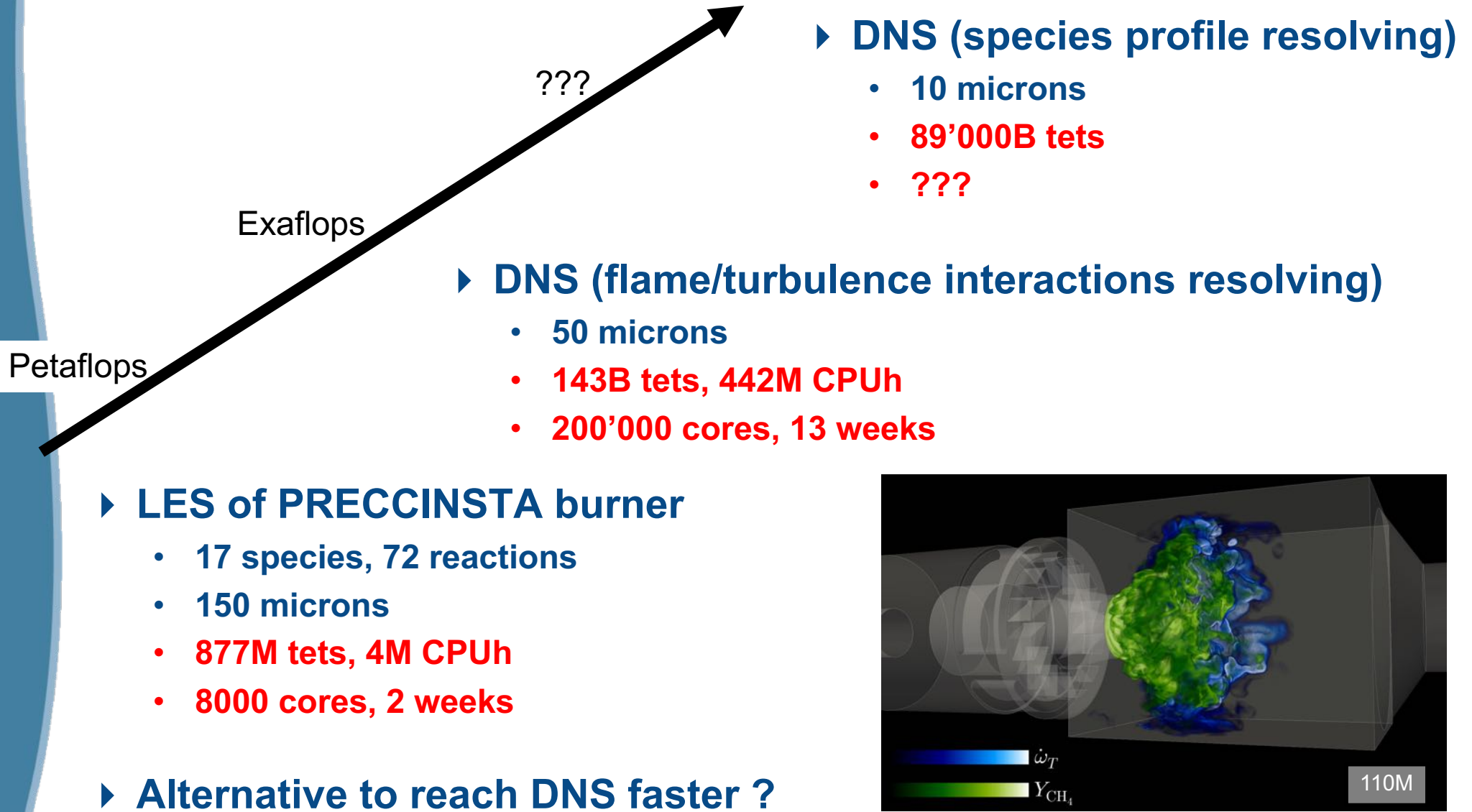
# Mean and RMS CO mass fraction



## ► Some error on CO remain due to TFLES combustion model



# When can we expect a DNS of PRECCINSTA? (or of lab-scale burners)



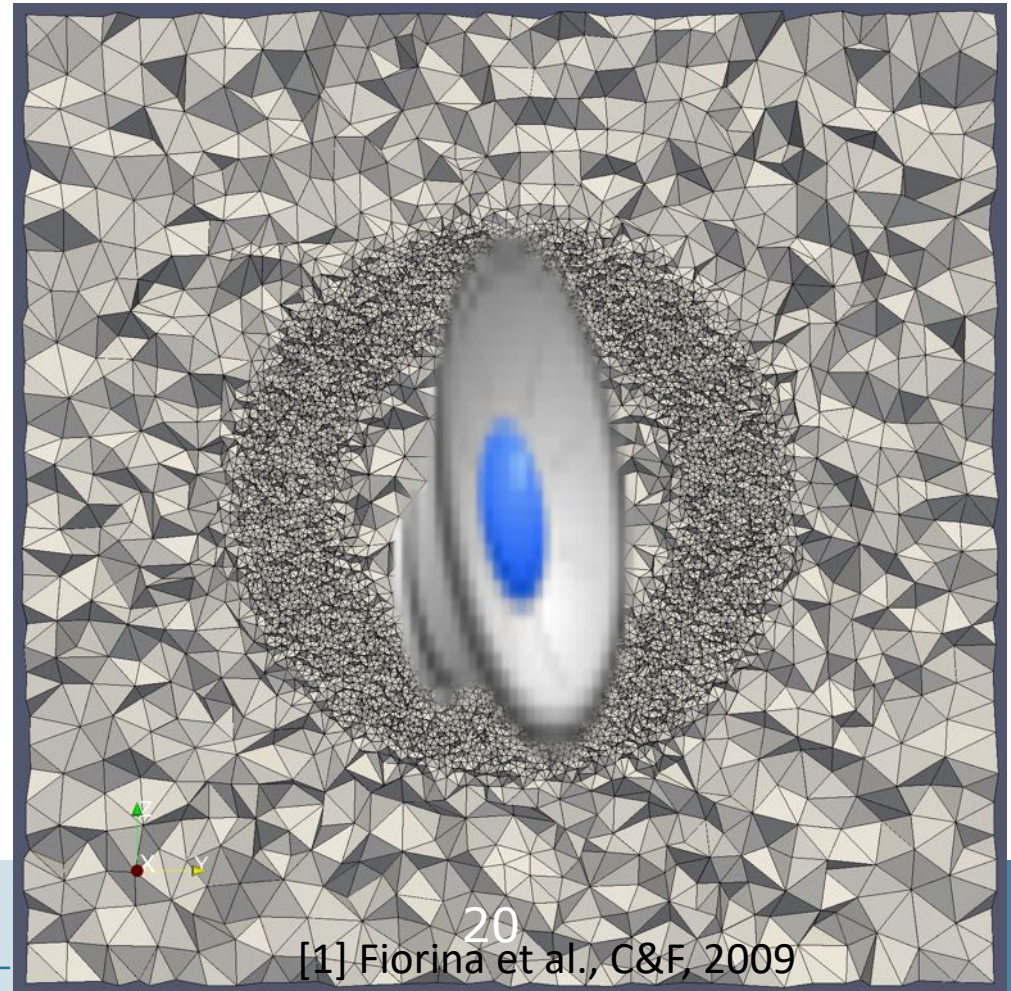
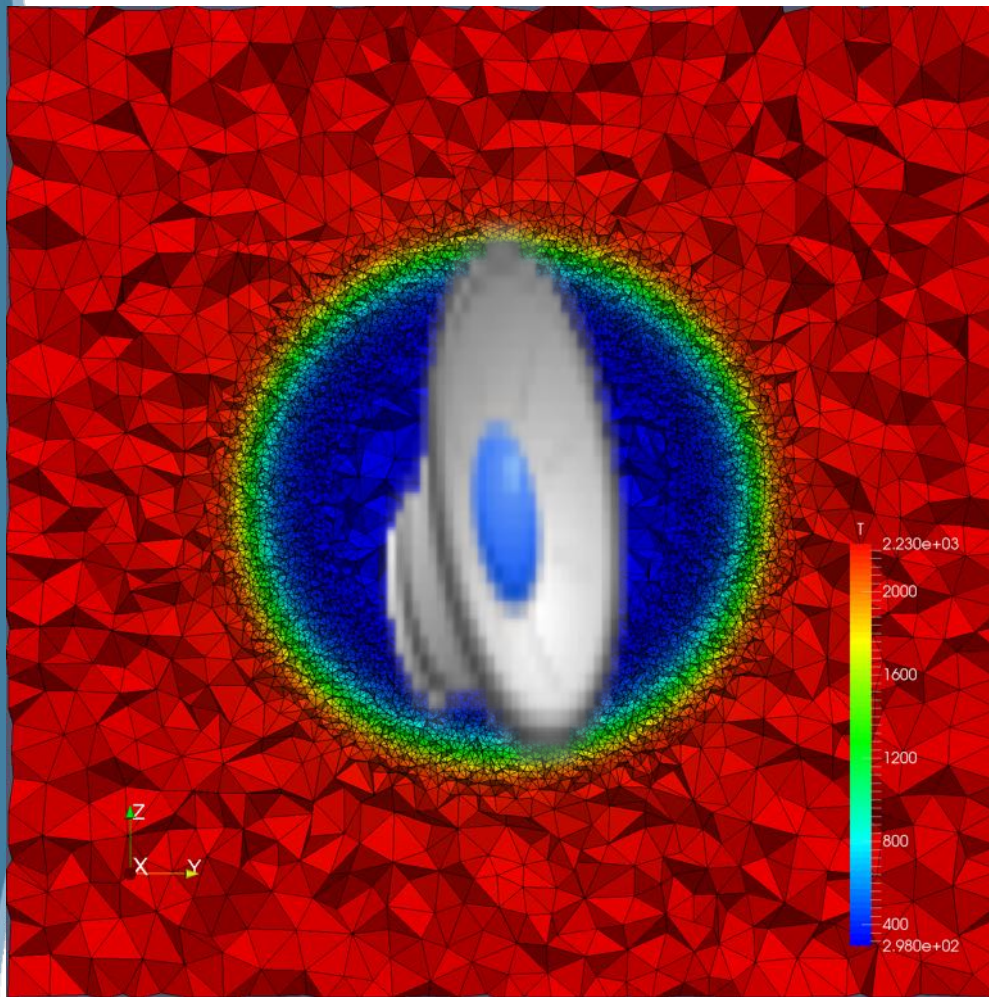


# ■ Dynamic h-adaptation of a premixed flame

- ▶ F-TACLES combustion model [1], refinement ratio = 6
- ▶ H-adaptation performed with the MMG library from INRIA
- ▶ More details in Bénard et al., IJNMF, 2015



[www.mmgtools.org](http://www.mmgtools.org)

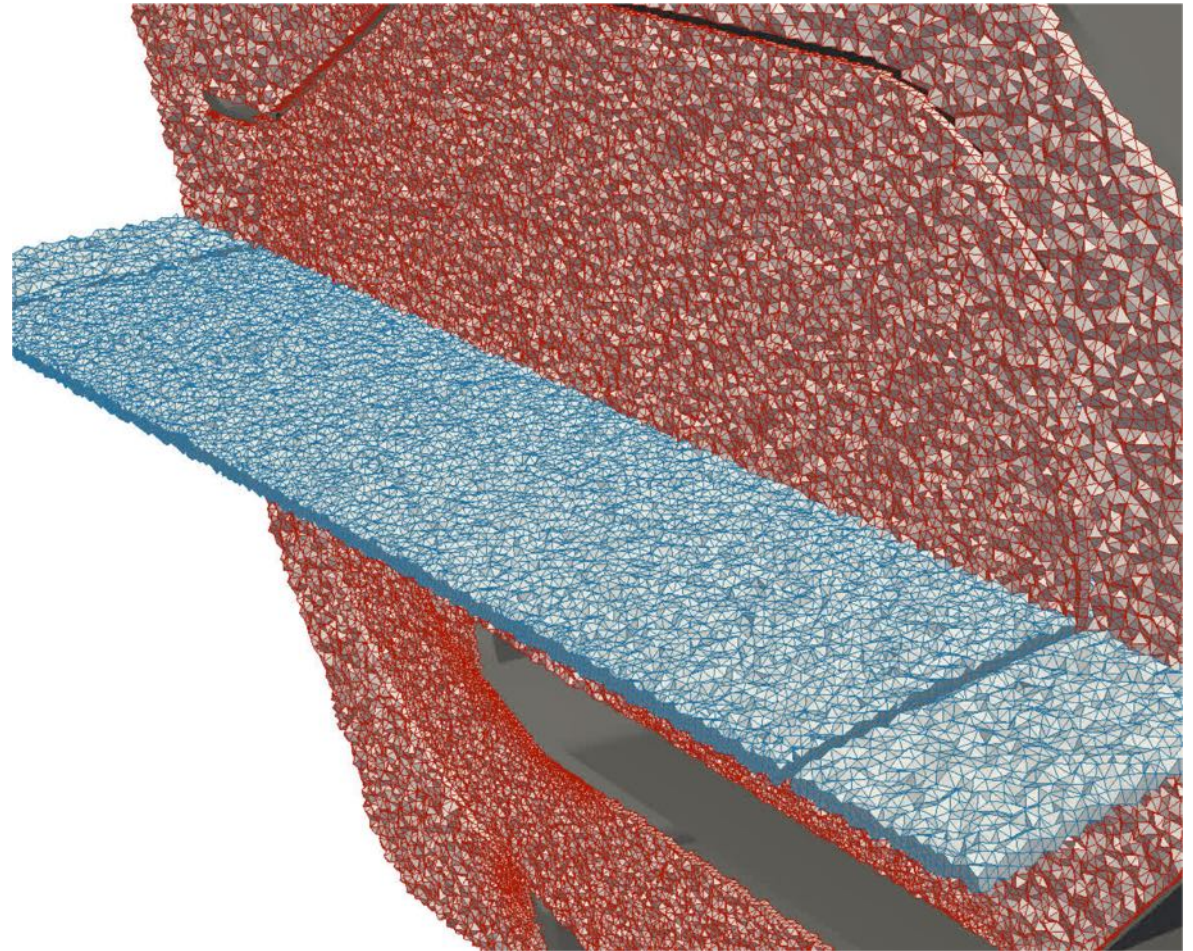


20  
[1] Fiorina et al., C&F, 2009



# ■ Application: Ignition in a SAFRAN HE combustor

- SAFRAN Tech simulation (R. Mercier)
- F-TACLES model with variable filter width
- Iso-temperature at 1300K colored by vorticity
- Parameters
  - Refinement ratio = 5
  - 41M to 75M tets
  - Physical duration = 0.3 ms
  - 5h on 512 Cobalt cores
  - 1 adaptation every 15 iter.
  - 1 adaptation = 4 minutes
  - Adaptation cost = 50%

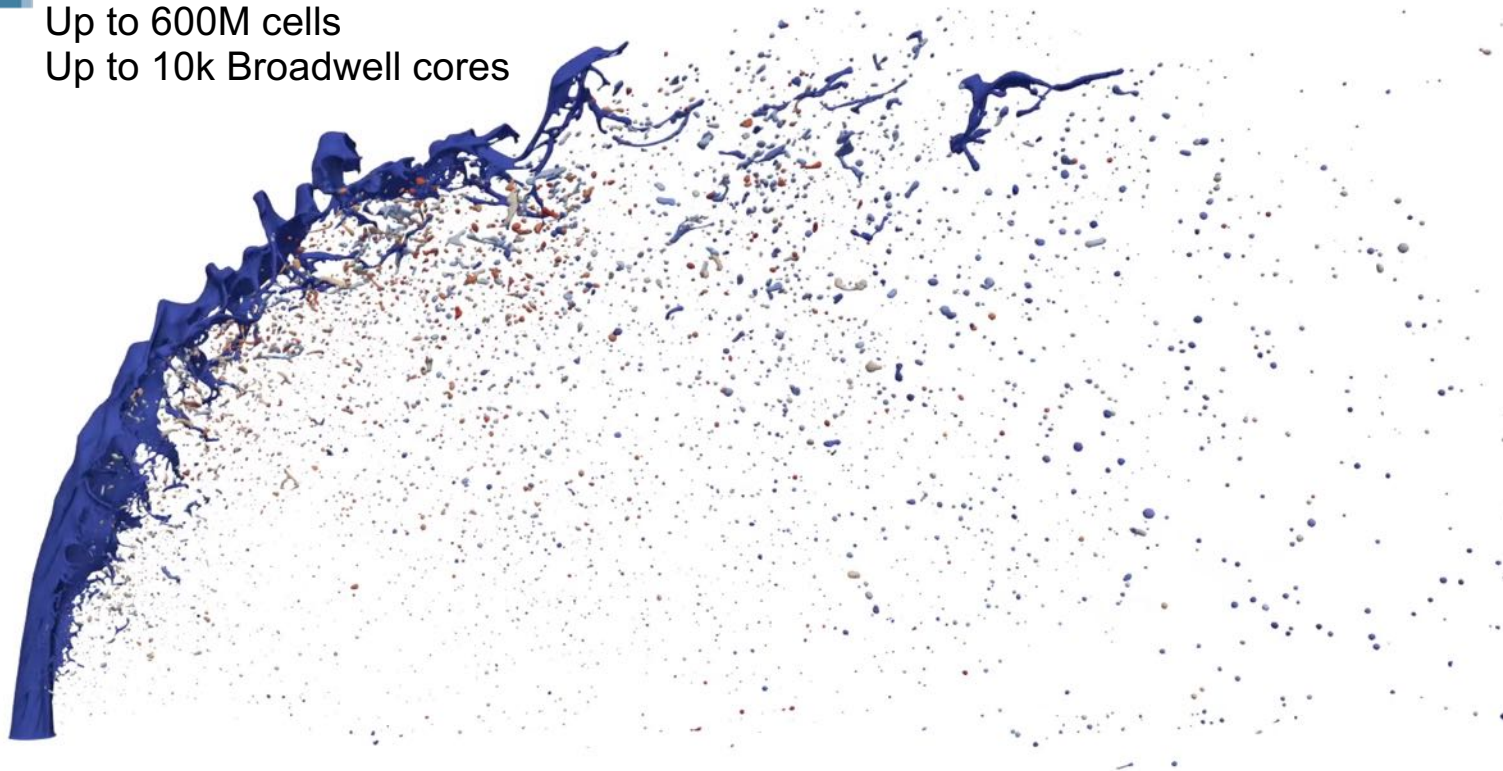


**On-going simulations with periodic dynamic remeshing by G. Vaudor**

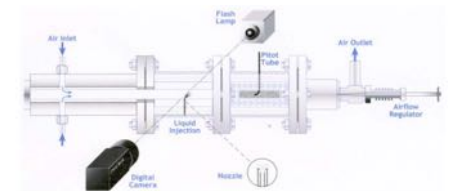
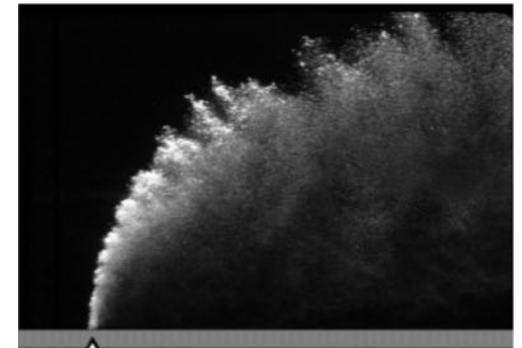
# Primary atomization of a jet-in-cross-flow

## ► Kerosene jet in air at 10 bar

10 microns at the interface  
Up to 600M cells  
Up to 10k Broadwell cores



Ragucci et al. 2007  
Atomization & Sprays



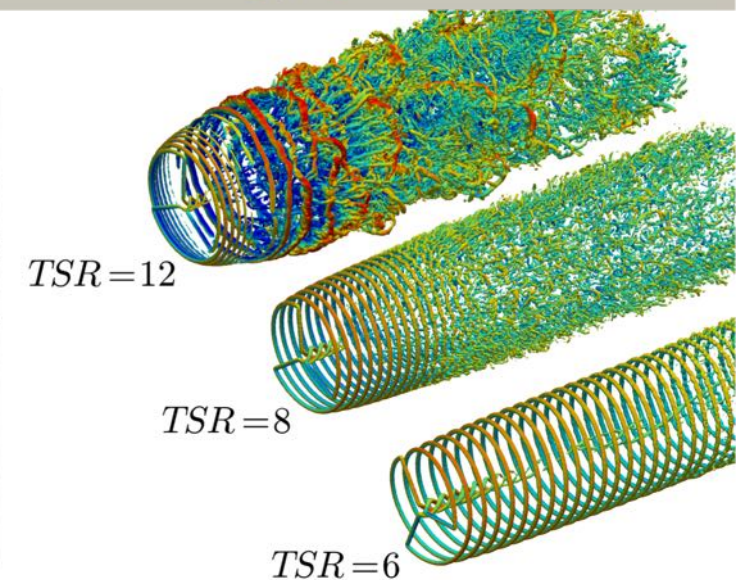
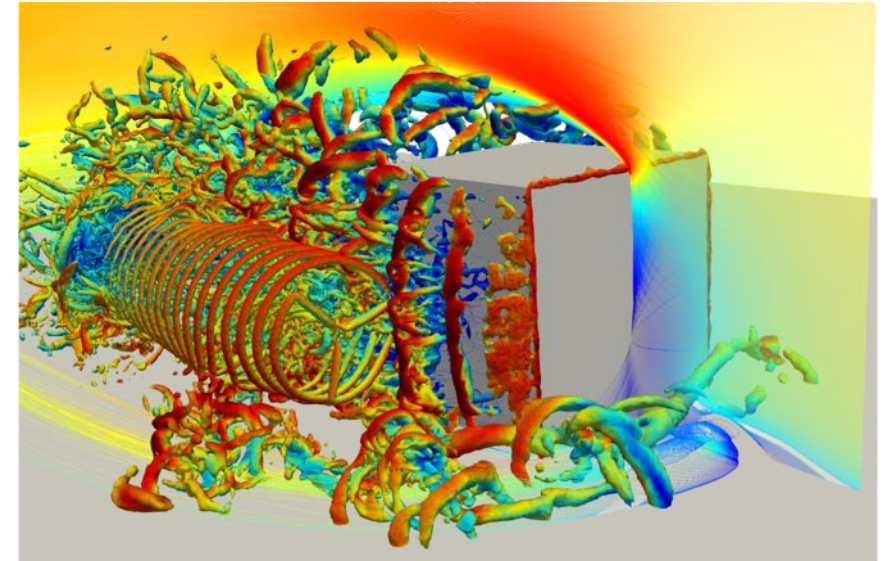
- Injector diameter:  $D=0.5$  mm
- Flow section: 25 mm x 25 mm
- **Pressure: 10 bars**
- $V_{\text{air}} = 37$  m/s and  $V_{\text{kerosene}} = 17$  m/s
- $Re_{\text{air}} = 590$  287 and  $Re_{\text{kero}} = 4477$
- $We_{\text{aero}} = \rho_{\text{air}} V_{\text{kero}}^2 D / \sigma = 63.5$
- $q = \rho_{\text{kero}} V_{\text{kero}}^2 / \rho_{\text{air}} V_{\text{air}}^2 = 14.2$

Dynamic mesh adaptation of a kerosene jet in cross flow. J. Leparoux, H. Musaefendic, R. Mercier, V. Moureau, accepted to ICLASS 2018, Chicago.



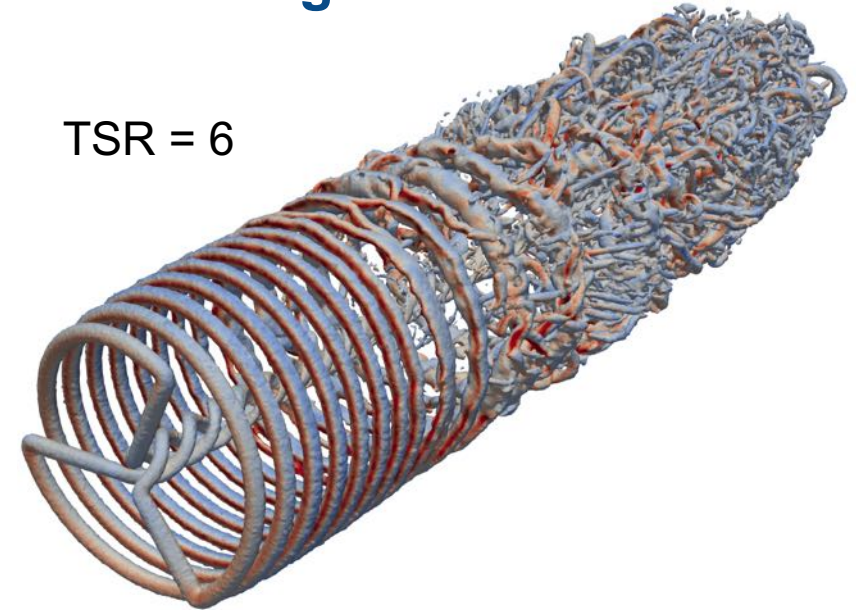
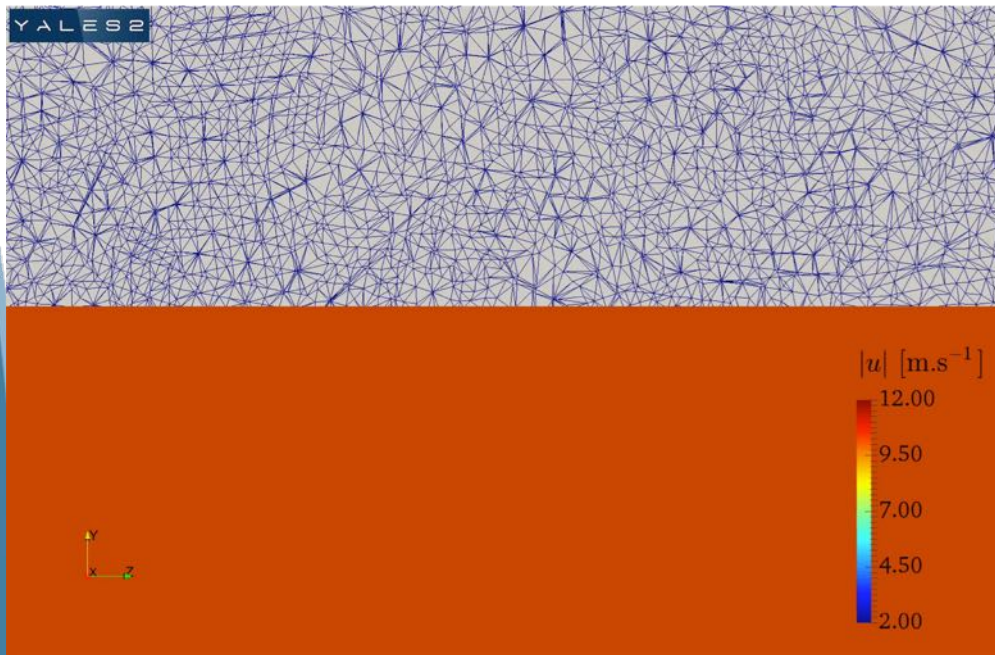
# ■ Application to wind turbines

- ▶ Modeling of wind turbine wakes is important to evaluate wind farm effects on the rotor loading
  - Becomes critical when reaching 10MW and 200m diameter rotors
- ▶ LES-actuator line framework
  - Based on unstructured grids
  - Takes into account any geometric detail
  - Bénard et al., Comp. Fluids, 2018



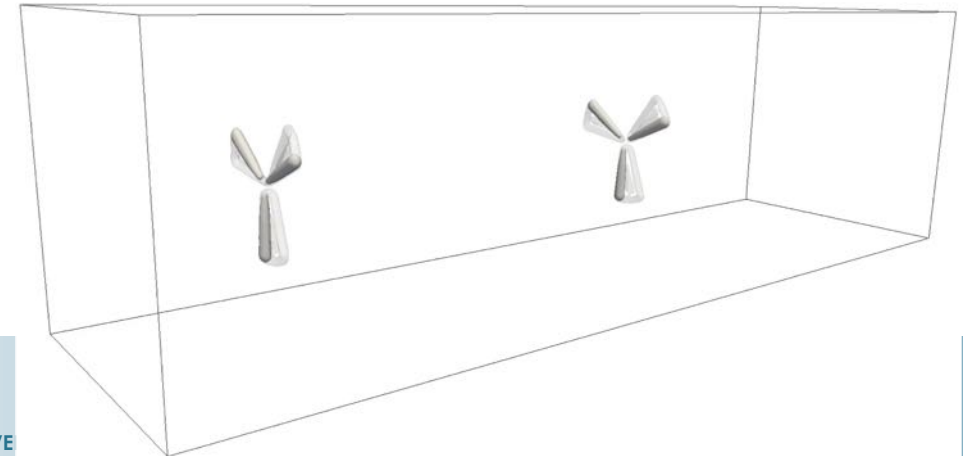
# ■ Application to wind turbines

- ▶ H-adaptation refinement criterion based on local vorticity
- ▶ Enables to reach unprecedented precision for a given cell count



YALES2 coRia INSA Adwen NORMANDIE

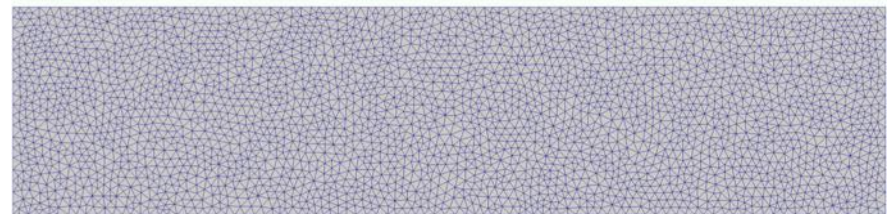
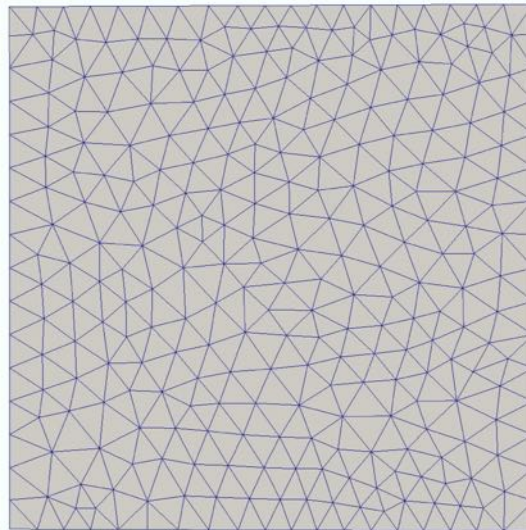
**Ultimately: application to wind turbine interactions**





# ■ Conclusions

- ▶ **LES of complex burners with finite-rate chemistry becomes feasible**
  - On-going PRACE simulations with GRI3 mechanism (52 species, 300+ reactions)
- ▶ **Dynamic mesh adaptation is a solution to achieve more accuracy for a given cell count**
- ▶ **Many developments are still required to be widely applied**
  - Surface remeshing



# Acknowledgments

- PhDs and postdocs of the YALES2 team
- R. Mercier - SAFRAN Tech, France
- C. Dobrzynski, A. Froehly – IMB/INRIA Bordeaux, France
- A. Pushkarev, G. Balarac – LEGI, Grenoble, France
- L. Bricteux and his team, UMONS, Belgium
- CPU hours from PRACE, GENCI and CRIANN

